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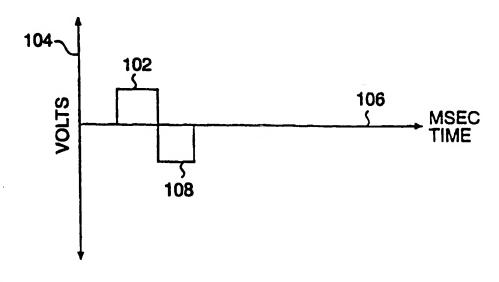
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09/008,636 16 January 1998 (16.01.98) US (71)(72) Applicant and Inventor: MOWER, Morton, M. [US/US]; 3908 North Charles Street #1001, Baltimore, MD 21218 (US). (74) Agent: ROBERTS, Jon, L.; Roberts & Brownell, LLC, Suite 212, 8381 Old Courthouse Road, Vienna, VA 22182 (US).	SI, SK, SL, TJ, TM, TR, TT, UA, UG, US, UZ, VN, YUZW, ARIPO patent (GH, GM, KE, LS, MW, SD, SZ, UGZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FF, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI pater (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE SN, TD, TG).

(54) Title: AUGMENTATION OF ELECTRICAL CONDUCTION AND CONTRACTIBILITY BY BIPHASIC CARDIAC PACING ADMINISTERED VIA THE CARDIAC BLOOD POOL



(57) Abstract

Augmentation of electrical conduction and contractibility by biphasic cardiac pacing. A first stimulation phase is administered to the cardiac blood pool. This first stimulation phase has a predefined polarity, amplitude and duration. A second stimulation phase is then administered to the cardiac blood pool. This second phase also has a predefined polarity, amplitude and duration. The two phases are applied sequentially. Contrary to current thought, anodal stimulation is first applied and followed by cathodal stimulation. In this fashion, pulse conduction through the cardiac muscle is improved together with the increase in contractibility.

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1	AUGMENTATION OF ELECTRICAL CONDUCTION AND CONTRACTILITY BY
2	BIPHASIC CARDIAC PACING ADMINISTERED VIA THE CARDIAC BLOOD
3	<u>POOL</u>
4	Inventor: Morton M. Mower, M.D.
5	
6	RELATED APPLICATION DATA
7	
8	The present disclosure is a continuation-in-part application related to the U.S. Patent
9	Application entitled "Augmentation of Electrical Conduction and Contractility by Biphasic
10	Cardiac Pacing", Serial No. 08/699,552, filed August 8, 1996.
11	
12	FIELD OF THE INVENTION
13	
14	This invention relates generally to a method for the stimulation of muscle tissue. In
15	particular, this invention relates to a method for cardiac stimulation and pacing with biphasic
16	waveforms wherein the stimulation is administered via the cardiac blood pool.
17	
18	BACKGROUND OF THE INVENTION
19	
20	The function of the cardiovascular system is vital for survival. Through blood
21	circulation, body tissues obtain necessary nutrients and oxygen, and discard waste substances
22	In the absence of circulation, cells begin to undergo irreversible changes that lead to death.
23	The muscular contractions of the heart are the driving force behind circulation.
24	In cardiac muscle, the muscle fibers are interconnected in branching networks that
25	spread in all directions through the heart. When any portion of this net is stimulated, a
26	depolarization wave passes to all of its parts and the entire structure contracts as a unit.
27	Before a muscle fiber can be stimulated to contract, its membrane must be polarized. A
28	muscle fiber generally remains polarized until it is stimulated by some change in its
29	environment. A membrane can be stimulated electrically, chemically, mechanically or by
30	temperature change. The minimal stimulation strength needed to elicit a contraction is

known as the threshold stimulus. The maximum stimulation amplitude that may be administered without eliciting a contraction is the maximum subthreshold amplitude.

Where the membrane is stimulated electrically, the impulse amplitude required to elicit a response is dependent upon a number of factors. First, is the duration of current flow. Since the total charge transferred is equal to the current amplitude times the pulse duration, increased stimulus duration is associated with a decrease in threshold current amplitude. Second, the percentage of applied current that actually traverses the membrane varies inversely with electrode size. Third, the percentage of applied current that actually traverses the membrane varies directly with the proximity of the electrode to the tissue. Fourth, the impulse amplitude required to elicit a response is dependent upon the timing of stimulation within the excitability cycle.

Throughout much of the heart are clumps and strands of specialized cardiac muscle tissue. This tissue comprises the cardiac conduction system and serves to initiate and distribute depolarization waves throughout the myocardium. Any interference or block in cardiac impulse conduction may cause an arrhythmia or marked change in the rate or rhythm of the heart

Sometimes a patient suffering from a conduction disorder can be helped by an artificial pacemaker. Such a device contains a small battery powered electrical stimulator. When the artificial pacemaker is installed, electrodes are generally threaded through veins into the right ventricle, or into the right atrium and right ventricle, and the stimulator is planted beneath the skin in the shoulder or abdomen. The leads are planted in intimate contact with the cardiac tissue. The pacemaker then transmits rhythmic electrical impulses to the heart, and the myocardium responds by contracting rhythmically. Implantable medical devices for the pacing of the heart are well known in the art and have been used in humans since approximately the mid 1960s.

Either cathodal or anodal current may be used to stimulate the myocardium. However anodal current is thought not to be useful clinically. Cathodal current comprises electrical pulses of negative polarity. This type of current depolarizes the cell membrane by discharging the membrane capacitor, and directly reduces the membrane potential toward threshold level. Cathodal current, by directly reducing the resting membrane potential toward threshold has a one-half to one-third lower threshold current in late diastole than does anodal

current. Anodal current comprises electrical pulses of positive polarity. The effect of anodal current is to hyperpolarize the resting membrane. On sudden termination of the anodal pulse, the membrane potential returns towards resting level, overshoots to threshold, and a propagated response occurs. The use of anodal current to stimulate the myocardium is generally discouraged due to the higher stimulation threshold, which leads to use of a higher current, resulting in a drain on the battery of an implanted device and impaired longevity. Additionally, the use of anodal current for cardiac stimulation is discouraged due to the suspicion that the anodal contribution to depolarization can, particularly at higher voltages, contribute to arrhythmogenesis.

Virtually all artificial pacemaking is done using stimulating pulses of negative polarity, or in the case of bipolar systems, the cathode is closer to the myocardium than is the anode. Where the use of anodal current is disclosed, it is generally as a charge of minute magnitude used to dissipate residual charge on the electrode. This does not affect or condition the myocardium itself. Such a use is disclosed in U.S. Patent No. 4,543,956 to Herscovici.

The use of a triphasic waveform has been disclosed in U.S. Patent Nos. 4,903,700 and 4,821,724 to Whigham et al., and U.S. Patent No. 4,343,312 to Cals et al. Here, the first and third phases have nothing to do with the myocardium per se, but are only envisioned to affect the electrode surface itself. Thus, the charge applied in these phases is of very low amplitude.

Lastly, biphasic stimulation is disclosed in U.S. Patent No. 4,402,322 to Duggan. The goal of this disclosure is to produce voltage doubling without the need for a large capacitor in the output circuit. The phases of the biphasic stimulation disclosed are of equal magnitude and duration.

What is needed is an improved means for stimulating muscle tissue, wherein the contraction elicited is enhanced and the damage to the tissue adjacent to the electrode is diminished.

Enhanced myocardial function is obtained through the biphasic pacing of the present invention. The combination of cathodal with anodal pulses of either a stimulating or conditioning nature, preserves the improved conduction and contractility of anodal pacing while eliminating the drawback of increased stimulation threshold. The result is a depolarization wave of increased propagation speed. This increased propagation speed

results in superior cardiac contraction leading to an improvement in blood flow. Improved stimulation at a lower voltage level also results in reduction in power consumption and increased life for pacemaker batteries. Lastly, the improved stimulation achieved through the practice of the present invention allows for cardiac stimulation without the necessity of placing electrical leads in intimate contact with cardiac tissue. Standard stimuli delivered to the cardiac blood pool are ineffective in capturing the myocardium because it does not meet the stimulation threshold. While voltage of the pulse generator can be increased, when it does capture it is often so high that it also stimulates skeletal muscles thereby causing a painful twitching of the chest wall when only the heart stimulation was desired. As will be further discussed, through the practice of the present invention, one can enhance myocardial function through cardiac blood pool stimulation.

As with the cardiac muscle, striated muscle may also be stimulated electrically, chemically, mechanically or by temperature change. Where the muscle fiber is stimulated by a motor neuron, the neuron transmits an impulse which activates all of the muscle fibers within its control, that is, those muscle fibers in its motor unit. Depolarization in one region of the membrane stimulates adjacent regions to depolarize also, and a wave of depolarization travels over the membrane in all directions away from the site of stimulation. Thus, when a motor neuron transmits an impulse, all the muscle fibers in its motor unit are stimulated to contract simultaneously. The minimum strength to elicit a contraction is called the threshold stimulus. Once this level of stimulation has been met, the generally held belief is that increasing the level will not increase the contraction. Additionally, since the muscle fibers within each muscle are organized into motor units, and each motor unit is controlled by a single motor neuron, all of the muscle fibers in a motor unit are stimulated at the same time. However, the whole muscle is controlled by many different motor units that respond to different stimulation thresholds. Thus, when a given stimulus is applied to a muscle, some motor units may respond while others do not.

The combination of cathodal and anodal pulses of the present invention also provides improved contraction of striated muscle where electrical muscular stimulation is indicated due to neural or muscular damage. Where nerve fibers have been damaged due to trauma or disease, muscle fibers in the regions supplied by the damaged nerve fiber tend to undergo atrophy and waste away. A muscle that cannot be exercised may decrease to half of its usual

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size in a few months. Where there is no stimulation, not only will the muscle fibers decrease in size, but they will become fragmented and degenerated, and replaced by connective tissue. Through electrical stimulation one may maintain muscle tone, such that upon healing or regeneration of the nerve fiber, viable muscle tissue remains. Enhanced muscle contraction is obtained through the biphasic stimulation of the present invention. The combination of cathodal with anodal pulses of either a stimulating or conditioning nature results in contraction of a greater number of motor units at a lower voltage level, leading to superior muscle response. SUMMARY OF THE INVENTION It is therefore an object of the present invention to provide improved stimulation of cardiac tissue. It is another object of the present invention to increase cardiac output through superior cardiac contraction leading to greater stroke volume. It is another object of the present invention to increase impulse propagation speed. It is another object of the present invention to extend pacemaker battery life. It is a further object of the present invention to obtain effective cardiac stimulation at a lower voltage level. It is a further object of the present invention to eliminate the necessity of placing electrical leads in intimate contact with tissue to obtain tissue stimulation. It is a further object of the present invention to provide improved stimulation of muscle tissue. It is a further object of the present invention to provide contraction of a greater 24 number of muscle motor units at a lower voltage level. 25 A method and apparatus for muscular stimulation in accordance with the present 26 invention includes the administration of biphasic stimulation to the muscle tissue, wherein 27 both cathodal and anodal pulses are administered. According to one aspect of this invention, 28 this stimulation is administered to the myocardium in order to enhance myocardial function.

According to a further aspect of this invention, this stimulation is administered to the cardiac

blood pool and thereafter conducted to the cardiac tissue. This enables cardiac stimulation

without the necessity of placing electrical leads in intimate contact with cardiac tissue.

According to a still further aspect of this invention, the stimulation is administered to striated muscle tissue to evoke muscular response. Pacemaker electronics needed to practice the method of the present invention are well known to those skilled in the art. Current pacemaker electronics are capable of being programmed to deliver a variety of pulses, including those disclosed herein.

The method and apparatus of the present invention comprises a first and second stimulation phase, with each stimulation phase having a polarity, amplitude, shape and duration. In a preferred embodiment the first and second phases have differing polarities. In one alternative embodiment, the two phases are of differing amplitude. In a second alternative embodiment, the two phases are of differing duration. In a third alternative embodiment, the first phase is in a chopped wave form. In a fourth alternative embodiment, the amplitude of the first phase is ramped. In a fifth alternative embodiment the first phase is administered over 200 milliseconds after completion of a cardiac beating/pumping cycle. In a preferred alternative embodiment, the first phase of stimulation is an anodal pulse at maximum subthreshold amplitude for a long duration, and the second phase of stimulation is a cathodal pulse of short duration and high amplitude. It is noted that the aforementioned alternative embodiments can be combined in differing fashions. It is also noted that these alternative embodiments are intended to be presented by way of example only, and are not limiting.

BRIEF DESCRIPTION OF THE DRAWINGS

- Fig. 1 is a schematic representation of leading anodal biphasic stimulation.
- Fig. 2 is a schematic representation of leading cathodal biphasic stimulation.
- 25 Fig. 3 is a schematic representation of leading anodal stimulation of low level and long
- duration, followed by conventional cathodal stimulation.
- Fig. 4 is a schematic representation of leading anodal stimulation of ramped low level and
- long duration, followed by conventional cathodal stimulation.
- Fig. 5 is a schematic representation of leading anodal stimulation of low level and short
- duration, administered in series followed by conventional cathodal stimulation.

1 Fig. 6 graphs conduction velocity transverse to the fiber vs pacing duration resulting from 2 leading anodal biphasic pulse. Fig. 7 graphs conduction velocity parallel to the fiber vs pacing duration resulting from 3 4 leading anodal biphasic pulse. 5 6 DETAILED DESCRIPTION 7 8 The present invention relates to the biphasic electrical stimulation of muscle tissue. 9 Fig. 1 depicts biphasic electrical stimulation wherein a first stimulation phase comprising anodal 10 11 stimulus 102 is administered having amplitude 104 and duration 106. This first stimulation phase is immediately followed by a second stimulation phase comprising cathodal stimulation 12 108 of equal intensity and duration. 13 14 Fig. 2 depicts biphasic electrical stimulation wherein a first stimulation phase 15 comprising cathodal stimulation 202 having amplitude 204 and duration 206 is administered. 16 This first stimulation phase is immediately followed by a second stimulation phase 17 comprising anodal stimulation 208 of equal intensity and duration. 18 Fig. 3 depicts a preferred embodiment of the present invention wherein a first 19 stimulation phase comprising low level, long duration anodal stimulation 302 having amplitude 304 and duration 306 is administered. This first stimulation phase is immediately 20 followed by a second stimulation phase comprising cathodal stimulation 308 of conventional 21 22 intensity and duration. In an alternative embodiment of the invention, anodal stimulation 302 23 is at maximum subthreshold amplitude. In yet another alternative embodiment of the 24 invention, anodal stimulation 302 is less than three volts. In another alternative embodiment of the invention, anodal stimulation 302 is a duration of approximately two to eight 25 26 milliseconds. In yet another alternative embodiment of the invention, cathodal stimulation 27 308 is of a short duration. In another alternative embodiment of the invention, cathodal 28 stimulation 308 is approximately 0.3 to 0.8 milliseconds. In yet another alternative 29 embodiment of the invention, cathodal stimulation 308 is of a high amplitude. In another alternative embodiment of the invention, cathodal stimulation 308 is in the approximate range 30

of three to twenty volts. In yet another alternative embodiment of the present invention,

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cathodal stimulation 308 is of a duration less than 0.3 milliseconds and at a voltage greater than twenty volts. In another alternative embodiment, anodal stimulation 302 is administered over 200 milliseconds post heart beat. In the manner disclosed by these embodiments, as well as those alterations and modifications which may become obvious upon the reading of this specification, a maximum membrane potential without activation is achieved in the first phase of stimulation.

Fig. 4 depicts an alternative preferred embodiment of the present invention wherein a first stimulation phase comprising anodal stimulation 402 is administered over period 404 with rising intensity level 406. The ramp of rising intensity level 406 may be linear or nonlinear, and the slope may vary. This anodal stimulation is immediately followed by a second stimulation phase comprising cathodal stimulation 408 of conventional intensity and duration. In an alternative embodiment of the invention, anodal stimulation 402 rises to a maximum subthreshold amplitude. In yet another alternative embodiment of the invention, anodal stimulation 402 rises to a maximum amplitude that is less than three volts. In another alternative embodiment of the invention, anodal stimulation 402 is a duration of approximately two to eight milliseconds. In yet another alternative embodiment of the invention, cathodal stimulation 408 is of a short duration. In another alternative embodiment of the invention, cathodal stimulation 408 is approximately 0.3 to 0.8 milliseconds. In yet another alternative embodiment of the invention, cathodal stimulation 408 is of a high amplitude. In another alternative embodiment of the invention, cathodal stimulation 408 is in the approximate range of three to twenty volts. In yet another alternative embodiment of the present invention, cathodal stimulation 408 is of a duration less than 0.3 milliseconds and at a voltage greater than twenty volts. In another alternative embodiment, anodal stimulation 402 is administered over 200 milliseconds post heart beat. In the manner disclosed by these embodiments as well as those alterations and modifications which may become obvious upon the reading of this specification, a maximum membrane potential without activation is achieved in the first phase of stimulation.

Fig. 5 depicts biphasic electrical stimulation wherein a first stimulation phase comprising series 502 of anodal pulses is administered at amplitude 504. In one embodiment rest period 506 is of equal duration to stimulation period 508 and is administered at baseline amplitude. In an alternative embodiment, rest period 506 is of a differing duration than

stimulation period 508 and is administered at baseline amplitude. Rest period 506 occurs after each stimulation period 508 with the exception that a second stimulation phase comprising cathodal stimulation 510 of conventional intensity and duration immediately follows the completion of series 502. In an alternative embodiment of the invention, the total charge transferred through series 502 of anodal stimulation is at the maximum subthreshold level. In yet another alternative embodiment of the invention, the first stimulation pulse of series 502 is administered over 200 milliseconds post heart beat. In another alternative embodiment of the invention, cathodal stimulation 510 is of a short duration. In yet another alternative embodiment of the invention, cathodal stimulation 510 is approximately 0.3 to 0.8 milliseconds. In another alternative embodiment of the invention, cathodal stimulation 510 is in the approximate range of three to twenty volts. In another alternative embodiment of the invention, cathodal stimulation 510 is of a duration less than 0.3 milliseconds and at a voltage greater than twenty volts.

EXAMPLE 1

Stimulation and propagation characteristics of the myocardium were studied in isolated hearts using pulses of differing polarities and phases. The experiments were carried out in five isolated Langendorff perfused rabbit hearts. Conduction velocity on the epicardium was measured using an array of bipolar electrodes. Measurements were made between six millimeters and nine millimeters from the stimulation site. Transmembrane potential was recorded using a floating intracellular microelectrode. The following protocols were examined: monophasic cathodal pulse, monophasic anodal pulse, leading cathodal biphasic pulse and leading anodal biphasic pulse.

Table 1 discloses the conduction speed transverse to fiber direction for each stimulation protocol administered, with stimulations of three, four and five volts and two millisecond pulse duration.

1		TABLE 1		
1 2		Conduction Speed Tr	ansverse to Fiber Direc	ction, 2 msec
3	duration	•		
4	diamon	3 V	4 V	5 V
5 6 7 8	Cathodal Monophasic Anodal Monophasic Leading Cathodal Biphasic Leading Anodal Biphasic	18.9 ± 2.5 cm/sec 24.0 ± 2.3 cm/sec 27.1 ± 1.2 cm/sec 26.8 ± 2.1 cm/sec	21.4 ± 2.6 cm/sec 27.5 ± 2.1 cm/sec 28.2 ± 2.3 cm/sec 28.5 ± 0.7 cm/sec	23.3 ± 3.0 cm/sec 31.3 ± 1.7 cm/sec 27.5 ± 1.8 cm/sec 29.7 ± 1.8 cm/sec
9	Table 2 discloses the	conduction speed alor	ng fiber direction for ea	ach stimulation
10	protocol administered, with			
11	_			
12	pulse duration.			
13		TABLE	2	
14			Along Fiber Direction,	2 msec stimulation
15 16		3 V	4 V	5 V
17 18 19 20 21	Cathodal Monophasic Anodal Monophasic Leading Cathodal Biphasic Leading Anodal Biphasic	45.3 ± 0.9 cm/sec 48.1 ± 1.2 cm/sec 50.8 ± 0.9 cm/sec 52.6 ± 2.5 cm/sec	47.4 ± 1.8 cm/sec 51.8 ± 0.5 cm/sec 52.6 ± 1.1 cm/sec 55.3 ± 1.5 cm/sec	49.7 ± 1.5 cm/sec 54.9 ± 0.7 cm/sec 52.8 ± 1.7 cm/sec 54.2 ± 2.3 cm/sec
22	The differences in c	onduction velocities b	etween the cathodal me	onophasic, anodal
23	monophasic, leading cathod	lal biphasic and leadin	ng anodal biphasic were	e found to be
24	significant (p < 0.001). From	m the transmembrane	potential measurement	s, the maximum
25	upstroke ((dV/dt)max) of the	ne action potentials wa	as found to correlate we	ell with the changes in
26	conduction velocity in the l	ongitudinal direction.	For a four volt pulse of	of two millisecond
27	duration, (dV/dt)max was (63.5 ± 2.4 V/sec for ca	athodal and 75.5 ± 5.6	V/sec for anodal
28	pulses.			
29				
30	EXAMPLE 2			
31				
32	The effects of vary	ing pacing protocols o	on cardiac electrophysic	ology were analyzed
33	using Langendorff prepare			
34	constant voltage rectangul	ar pulse. The following	ng protocols were exar	nined: monophasic

anodal pulse, monophasic cathodal pulse, leading anodal biphasic pulse and leading cathodal biphasic pulse. Administered voltage was increased in one volt steps from one to five volts for both anodal and cathodal stimulation. Duration was increased in two millisecond steps from two to ten milliseconds. Epicardial conduction velocities were measured along and transverse to the left ventricular fiber direction at a distance between three to six millimeters from the left ventricular free wall. Figs. 6 and 7 depict the effects of stimulation pulse duration and the protocol of stimulation administered on the conduction velocities.

Fig. 6 depicts the velocities measured between three millimeters and six millimeters transverse to the fiber direction. In this region, cathodal monophasic stimulation 602 demonstrates the slowest conduction velocity for each stimulation pulse duration tested. This is followed by anodal monophasic stimulation 604 and leading cathodal biphasic stimulation 606. The fastest conductive velocity is demonstrated by leading anodal biphasic stimulation 608.

Fig. 7 depicts the velocities measured between three millimeters and six millimeters parallel to the fiber direction. In this region, cathodal monophasic stimulation 702 demonstrates the slowest conduction velocity for each stimulation pulse duration tested. Velocity results of anodal monophasic stimulation 704 and leading cathodal biphasic stimulation 706 are similar with anodal monophasic stimulation demonstrating slightly quicker speeds. The fastest conduction velocity is demonstrated by leading anodal biphasic stimulation 708.

In one aspect of the invention, electrical stimulation is administered to the cardiac muscle. The anodal stimulation component of biphasic electrical stimulation augments cardiac contractility by hyperpolarizing the tissue prior to excitation, leading to faster impulse conduction, more intracellular calcium release, and the resulting superior cardiac contraction. The cathodal stimulation component eliminates the drawbacks of anodal stimulation, resulting in effective cardiac stimulation at a lower voltage level than would be required with anodal stimulation alone. This in turn, extends pacemaker battery life and reduces tissue damage.

In a second aspect of the invention, biphasic electrical stimulation is administered to the cardiac blood pool, that is, the blood entering and surrounding the heart. This enables cardiac stimulation without the necessity of placing electrical leads in intimate contact with

 cardiac tissue, thereby diminishing the likelihood of damage to this tissue. The stimulation threshold of biphasic stimulation administered via the blood pool is in the same range as standard stimuli delivered directly to the heart muscle. Through the use of biphasic electrical stimulation to the cardiac blood pool it is therefore possible to achieve enhanced cardiac contraction, without skeletal muscle contraction, cardiac muscle damage or adverse effects to the blood pool.

In a third aspect of the invention biphasic electrical stimulation is applied to striated muscle tissue. The combination of anodal with cathodal stimulation results in the contraction of a greater number of muscular motor units at a lower voltage level, resulting in improved muscular response.

Having thus described the basic concept of the invention, it will be readily apparent to those skilled in the art that the foregoing detailed disclosure is intended to be presented by way of example only, and is not limiting. Various alterations, improvements and modifications will occur and are intended to those skilled in the art, but are not expressly stated herein. These modifications, alterations and improvements are intended to be suggested hereby, and within the spirit and scope of the invention. Further, the pacing pulses described in this specification are well within the capabilities of existing pacemaker electronics with appropriate programming. Accordingly, the invention is limited only by the following claims and equivalents thereto.

1	What is claim	ed is:
2	1.	A method for electrical cardiac pacing comprising:
3	applyi	ng electrical stimulation to a cardiac blood pool.
4	2.	The method for electrical cardiac pacing as in claim 1 wherein the electrical
5	stimulation co	omprises:
6	a first	stimulation phase with a first phase polarity, a first phase amplitude, a first
7	phase shape a	nd a first phase duration; and
8	a seco	nd stimulation phase with a second phase polarity, a second phase amplitude, a
9	second phase	shape and a second phase duration.
10	3.	The method for electrical cardiac pacing as in claim 2
11 -	where	in the first stimulation phase and the second stimulation phase are applied in
12	sequence to the	he cardiac blood pool.
13	4.	The method for electrical cardiac pacing of claim 2 wherein the first phase
14	polarity is po	ositive.
15	5.	The method for electrical cardiac pacing of claim 2 wherein the first phase
16	amplitude is	less than the second phase amplitude.
17	6.	The method for electrical cardiac pacing of claim 2 wherein the first phase
18	amplitude is	ramped from a baseline value to a second value.
19	7.	The method for electrical cardiac pacing of claim 6 wherein the second value
20	is equal to th	e second phase amplitude.
21	8.	The method for electrical cardiac pacing of claim 2 wherein the first
22	stimulation p	phase further comprises a series of stimulating pulses of a predetermined
23	amplitude, p	olarity and duration.
24	9.	The method for electrical cardiac pacing of claim 8 wherein the first
25	stimulation p	phase further comprises a series of rest periods.
26	10.	The method for electrical cardiac pacing of claim 9 wherein applying the first
27	stimulation p	phase further comprises applying a rest period of a baseline amplitude after at
28	least one stir	nulating pulse.

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11.

of equal duration to the duration of the stimulating pulse.

The method for electrical cardiac pacing of claim 10 wherein the rest period is

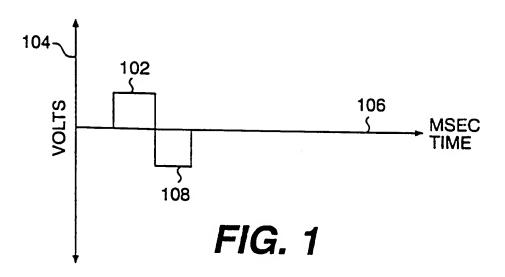
1	12.	The method for electrical cardiac pacing of claim 2 wherein the first phase
2	amplitude is a	at a maximum subthreshold amplitude.
3	13.	The method for electrical cardiac pacing of claim 12 wherein the maximum
4	subthreshold	amplitude is about 0.5 to 3.5 volts.
5	14.	The method for electrical cardiac pacing of claim 2 wherein the first phase
6	duration is at	least as long as the second phase duration.
7	15.	The method for electrical cardiac pacing of claim 2 wherein the first phase
8	duration is ab	out one to nine milliseconds.
9	16.	The method for electrical cardiac pacing of claim 2 wherein the second phase
10	duration is ab	out 0.2 to 0.9 milliseconds.
11	17.	The method for electrical cardiac pacing of claim 2 wherein the second phase
12	amplitude is	about two volts to twenty volts.
13	18.	The method for electrical cardiac pacing of claim 2 wherein the second phase
14	duration is le	ess than 0.3 milliseconds and the second phase amplitude is greater than 20 volts.
15	19.	The method for electrical cardiac pacing of claim 6 wherein the second value
16	is at a maxin	num subthreshold amplitude.
17	20.	The method for electrical cardiac pacing of claim 19 wherein the maximum
18	subthreshold	amplitude is about 0.5 to 3.5 volts.
19	21.	The method for electrical cardiac pacing of claim 6 wherein the first phase
20	duration is a	t least as long as the second phase duration.
21	22.	The method for electrical cardiac pacing of claim 6 wherein the first phase
22	duration is a	bout one to nine milliseconds.
23	23.	The method for electrical cardiac pacing of claim 6 wherein the second phase
24	duration is a	about 0.2 to 0.9 milliseconds.
25	24.	The method for electrical cardiac pacing of claim 6 wherein the second phase
26	amplitude is	s about two volts to twenty volts.
27	25.	The method for electrical cardiac pacing of claim 6 wherein the second phase
28	duration is	less than 0.3 milliseconds and the second phase amplitude is greater than 20 volts.
29	26.	The method for electrical cardiac pacing of claim 2 wherein the first
30	stimulation	phase is initiated greater than 200 milliseconds after completion of a cardiac

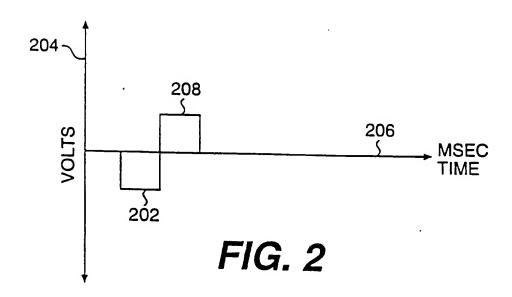
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beating cycle.

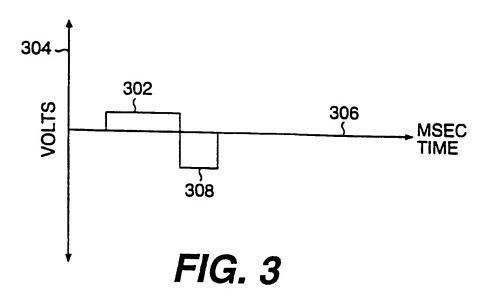
1	27. A method for electrical cardiac pacing comprising the steps of:
2	defining a first stimulation phase with a positive polarity, a first phase amplitude, a
3	first phase shape and a first phase duration, wherein said first phase amplitude is about 0.5 to
4	3.5 volts, wherein said first phase duration is about one to nine milliseconds and wherein sai
5	first stimulation phase is initiated greater than 200 milliseconds after completion of a cardiac
6	beating cycle;
7	defining a second phase with a negative polarity, a second phase amplitude, a second
8	phase shape and a second phase duration, wherein said second phase amplitude is about four
9	volts to twenty volts and wherein said second phase duration is about 0.2 to 0.9 millisecond
10	and
11	applying the first stimulation phase and the second stimulation phase in sequence to
12	the cardiac blood pool.
13	28. A method for electrical cardiac pacing comprising the steps of:
14	defining a first stimulation phase with a first phase polarity, a first phase amplitude,
15	first phase shape and a first phase duration;
16	defining a second phase with a second phase polarity, a second phase amplitude, a
17	second phase shape and a second phase duration; and
18	applying the first stimulation phase and the second stimulation phase in sequence to
19	the cardiac blood pool.

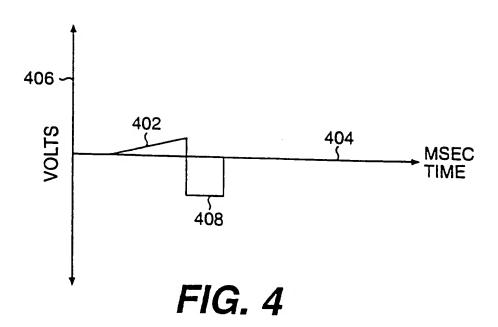
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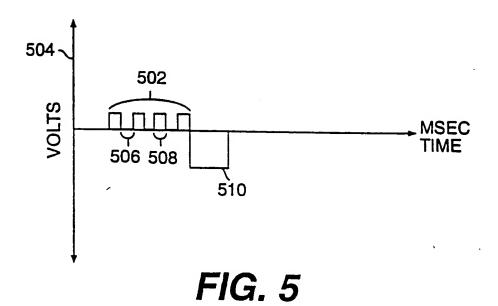


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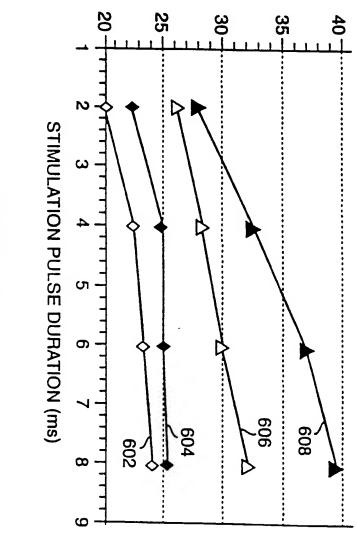


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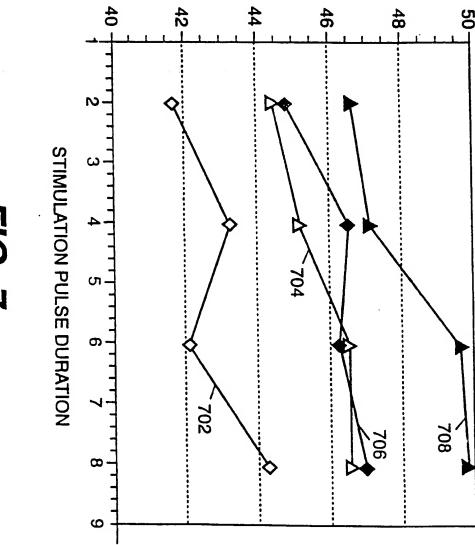
CONDUCTION VELOCITY (cm/s)



-1G. 6

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CONDUCTION VELOCITY (cm/s)



=1G. 7

Inte Ional Application No PCT/US 99/00879

a. classifi IPC 6	CATION OF SUBJECT MATTER A61N1/362		·
According to I	International Patent Classification (IPC) or to both national classification	on and IPC	
B. FIELDS S			
Minimum dood IPC 6	sumentation searched (classification system followed by classification $A61N$		
	on searched other than minimum documentation to the extent that suc ata base consulted during the international search (name of data base		
Electronic da	ala base consumed during the union about search fileline of data costs		
C. DOCUME	ENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the rele	vant passages	Relevant to claim No.
E	US 5 871 506 A (MOWER MORTON M) 16 February 1999 see the whole document		1,2
X	WO 97 25098 A (NEW TECHNOLOGIES SFENSTER MAIER (IL); BEN HAIM SHL 17 July 1997 see the whole document see page 9, line 28 - line 30 see page 14, line 14 - line 20 see page 19, line 12 - line 15 see page 33, line 7 - line 18 see page 34, line 12 - line 23	A YSY LTD OMO ()	1.2
[V] F1	unther documents are listed in the continuation of box C.	. Patent family members are liste	d in annex.
"A" docu con "E" eank tilin "L" docu wh cita "O" docu oth "P" docu	categories of cated documents: Iment delining the general state of the lart which is not sistered to be of particular relevance and document but published on or after the international grate grate international grate international grate international grate international grate international publication date of another control or other special reason (as specified) international referring to an oral disclosure, use, exhibition or the means ument published prior to the international filing date but are than the priority date claimed.	"T" later document published after the in or priority date and not in conflict will cited to understand the principle or invention. "X" document of particular relevance; the cannot be considered novel or cannot over the cannot be considered to involve an inventive step when the "Y" document of particular relevance; the cannot be considered to involve an document is combined with one or ments, such combination being down in the art. "8" document member of the same pate.	in the application but theory underlying the claimed invention not be considered to document is taken alone claimed invention inventive step when the more other such docurious to a person skilled
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Name a	nd mailing address of the ISA European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl.	Authonzed officer Ferrigno, A	

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Intit Jones Application No PCT/US 99/00879

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	ation) DOCUMENTS CONSIDERED TO BE RELEVANT				
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...emational application No.

PCT/US 99/00879

Box I Observations where certain claims were found unsearchable (Continuation of Item 1 of first sheet)
This International Search Report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:
1. X Claims Nos.: 3-28 because they relate to subject matter not required to be searched by this Authority, namely: Rule 39.1(iv) PCT- Method for treatment of the human or animal body by therapy: an incomplete search, within the limit of the available documentation, has been carried out for claims 1 and 2.
Claims Nos.: because they relate to parts of the International Application that do not comply with the prescribed requirements to such an extent that no meaningful International Search can be carried out, specifically:
3. Claims Nos.: because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).
Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)
This International Searching Authority found multiple inventions in this international application, as follows:
1. As all required additional search fees were timely paid by the applicant, this International Search Report covers all searchable claims.
As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.
3. As only some of the required additional search fees were timely paid by the applicant, this International Search Report covers only those claims for which fees were paid, specifically claims Nos.:
4. No required additional search fees were timely paid by the applicant. Consequently, this international Search Report is restricted to the invention first mentioned in the claims: it is covered by claims Nos.:
Remark on Protest The additional search fees were accompanied by the applicant's protest. No protest accompanied the payment of additional search fees.

Information on patent family members

Inte Ional Application No
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